

## PAPER

# Dependence of Elastic Modulus on Inner Pressure of Tube Wall Estimated from Measured Pulse Wave Velocity

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**SUMMARY** We have proposed a non-invasive method for diagnosis of the early stage of atherosclerosis, namely, the detection of small vibrations on the aortic wall near the heart by using ultrasound diagnostic equipment. It is, however, necessary to confirm the effectiveness of such measurement of the pulse wave velocity for quantitative evaluation of the local characteristics of atherosclerosis. It is well known that Young's modulus of a tube wall, estimated from measured pulse wave velocity, depends on inner pressure because of the non-linear relationship between the inner pressure and the change of volume in the tube. The inner pressure, however, changes during the period of one heart-beat. In this experimental study, we found for the first time that Young's modulus of the tube wall, estimated from the measured pulse wave velocity, depends not only on the diastolic pressure but also on the pulse pressure and the pressure gradient of the systolic period.

**Key words:** atherosclerosis, pulse wave velocity, elastic modulus, inner pressure

## 1. Introduction

We previously developed a noninvasive method to diagnose disorders of the cardiovascular system using ultrasound [1]. In the diagnosis of atherosclerosis, a major concern is changes in arterial wall hardness with every stage of this disease; such changes are determined by measuring the small vibrations which propagate on the artery. To date, in order to obtain an index for diagnosis of atherosclerosis, many investigators have measured the pulse wave velocity [2]. From the measured pulse wave velocity, Moens-Korteweg's equation [3] has been frequently applied to quantitative evaluation of the elastic modulus of the arterial wall. As is well known, the pulse wave is the pressure wave propagating in the cardiovascular system generated by beating of the heart. The propagation velocity  $c_0$  of the pulse wave is given by

$$c_0 = \sqrt{\frac{Eh}{2\rho r}}, \quad (1)$$

where  $E$  is Young's modulus of the arterial wall,  $\rho$  is the mass density of inner fluid,  $r$  is the inner radius of the artery, and  $h$  is the thickness of the arterial wall. Equation (1) implies that the pulse wave velocity  $c_0$  is proportional to the square root of Young's modulus  $E$  of the arterial wall. Hence, the stiffness of the arterial wall is quantitatively estimated by measuring the pulse wave velocity  $c_0$ . It is, however, necessary to make corrections since the pulse wave velocity  $c_0$  and then the obtained Young's modulus  $E$  of the arterial wall strongly depend on the inner pressure; the non-linear stress-strain relation of the aortic wall contributes to this dependence. In addition, the inner pressure changes its value during one cardiac cycle.

Numerous studies on the pulse wave and its propagation velocity  $c_0$  have been reported [2], [3]. The delay time of the pulse wave propagating between two measurement points, however, has been determined in the time domain and only rising time of the recorded pulse wave has been considered. It has been concluded that the pulse wave velocity  $c_0$  depends on only the dimensions of the cross sectional area and Young's modulus  $E$  of the arterial wall and the diastolic pressure [3]. To discuss the non-linear elastic characteristic of the arterial wall, it is insufficient to consider only the rising time of the pulse wave.

In this paper, the dependence of the pulse wave velocity  $c_0$  and obtained Young's modulus  $E$  on the inner pressure is experimentally evaluated by using a silicone rubber tube. Since the inner pressure varies during one cardiac cycle, not only the diastolic pressure but also the pulse pressure and the pressure gradient during systole are considered to be factors contributing to the pulse wave velocity  $c_0$  and Young's modulus  $E$ .

## 2. Methods

### 2.1 Measurement of Incremental Elastic Modulus $H$ for the Arterial Wall

In general, an arterial wall, which has incompressibil-

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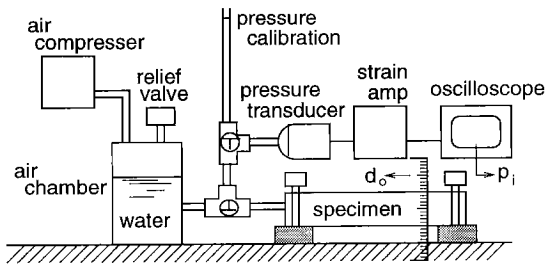


Fig. 1 Diagram showing testing of the relationship between the inner pressure  $p_i$  and the outer diameter  $d_o$ .

ity and a non-linear relationship between the stress and the strain with large amplitude, is an anisotropic viscoelastic medium. It is difficult to accurately describe the viscoelastic property of the arterial wall. Thus, the quantitative estimation of the elastic modulus of the arterial wall is of interest.

In our experiment, a silicone rubber tube is employed as a specimen. Its inner diameter and outer diameter are  $d_i = 11.8$  mm and  $d_o = 16.1$  mm, respectively, and its length is  $l = 243$  mm. Let us assume that the tube wall is an incompressible, uniform, isotropic, cylindrical elastic shell. In the case that tube length is constant (i.e. axial strain is negligible) by clamping both ends of tube, to quantitatively evaluate the stiffness of the tube wall, the following incremental elastic modulus  $H(p_i)$  [4] is employed:

$$H(p_i) = 2 \left( \frac{\Delta p_i}{\Delta d_o} \frac{d_o d_i^2}{d_o^2 - d_i^2} + \frac{p_i d_o^2}{d_o^2 - d_i^2} \right), \quad (2)$$

where  $p_i$  is the inner pressure,  $d_i$  and  $d_o$  are the inner diameter and the outer diameter of the artery, respectively, and  $\Delta p_i / \Delta d_o$  is the gradient of the pressure-diameter curve. The specimen has non-linearity on the stress-strain relationship. Hence, the value of  $H(p_i)$ , including the factor  $\Delta p_i / \Delta d_o$ , depends on the inner pressure  $p_i$ .

To obtain the incremental elastic modulus  $H(p_i)$  by using Eq. (2), the outer diameter  $d_o$  must be measured for various values of the inner pressure  $p_i$ . Figure 1 shows a schematic diagram for testing the relationship between the inner pressure  $p_i$  and the outer diameter  $d_o$ . Since it is assumed that the specimen has incompressibility, the inner diameter  $d_i$  is calculated from the measured outer diameter  $d_o$  by

$$d_i = \sqrt{d_o^2 - d_{o0}^2 + d_{i0}^2}, \quad (3)$$

where the subscript 0 indicates that the value is obtained when no inner pressure is applied ( $p_i = 0$ ).

## 2.2 Measurement of Pulse Wave Velocity $c_0$

We measure how the pulse wave velocity  $c_0$  and the obtained Young's modulus  $E$  vary when the inner pressure

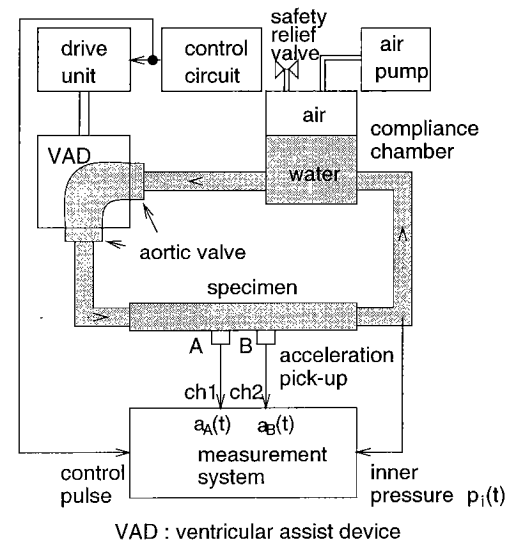


Fig. 2 A system for measurement of the pulse wave velocity using a ventricular assist device.

$p_i(t)$  is changed. Figure 2 shows a pulse wave measurement system [5]. In our measurement, signals  $a_A(t)$  and  $a_B(t)$  of the wall vibration generated by the pulse wave are simultaneously measured using two acceleration pickups which are attached to two adjacent points A and B on the wall surface of the specimen. From the resultant signals, the delay time  $\tau_{AB}$  of the pulse wave which propagates from point A to B is determined in the frequency domain by a computer. We concentrate on expansion of the tube wall in the systolic period, caused by an increase in the inner pressure  $p_i(t)$ . The time interval during the rise in pressure from the diastolic pressure to its peak is about 30 ms, and the Hamming window with 30 ms in time length is multiplied on the measured acceleration signals. The complex transfer function  $H_{AB}(f)$  from  $a_A(t)$  to  $a_B(t)$  and the magnitude-squared coherence function  $|\gamma_{AB}(f)|^2$  between  $a_A(t)$  and  $a_B(t)$  are obtained. When the pulse wave is non-dispersive, the phase  $\angle H_{AB}(f)$  of the transfer function varies linearly against the frequency  $f$ . Thus, the delay time  $\tau_{AB}$  is obtained from the gradient  $d\angle H_{AB}(f)/df$  of the phase of the transfer function, and the pulse wave velocity  $c_0$  is calculated by dividing the distance  $d_{AB}$  between the two points by the resultant delay time  $\tau_{AB}$ . The pulse wave velocity  $c_0$  is measured for various values of the diastolic pressure  $p_d = \min_t p_i(t)$ , the pulse pressure  $p_p = \max_t p_i(t) - \min_t p_i(t)$ , and the pressure gradient  $\partial p_i(t) / \partial t$  at systole.

## 3. Experimental Results

### 3.1 Incremental Elastic Modulus $H$

By changing the inner pressure  $p_i$ , the outer diameter  $d_o$  is measured at each pressure by using the system shown

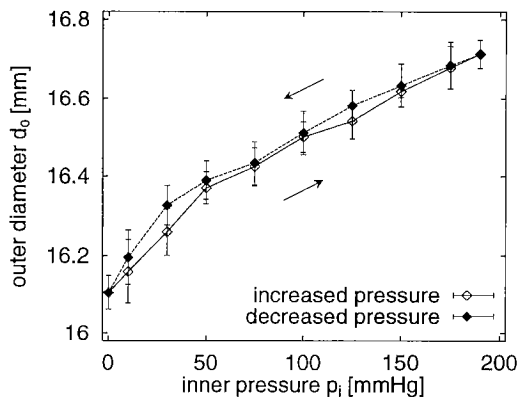


Fig. 3 Hysteretic elasticity of the silicone rubber tube.

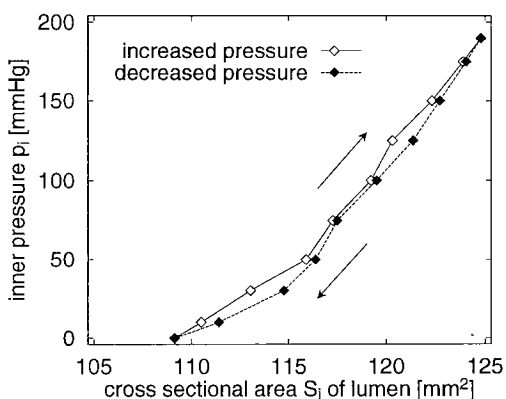


Fig. 4 Relationship between the inner pressure  $p_i$  and the cross sectional area  $S_i$  of the lumen.

in Fig. 1. The constant length condition is satisfied by clamping the specimen at both ends. The obtained relation between the inner pressure  $p_i$  and the outer diameter  $d_o$  is shown in Fig. 3. In this figure, each plot point shows the mean value and the error bar shows the standard deviation of 5-time measurements. The measurements have been done by using digital micrometer (SONY  $\mu$ -mate M-30) and the ratio of standard deviation to the mean value in 5-time measurements is less than 1%.

Figure 4 shows the hysteretic elasticity of the specimen, that is, the relationship between the inner pressure  $p_i$  on the vertical axis and the cross sectional area  $S_i$  of the lumen on the horizontal axis. By assuming incompressibility of the specimen,  $S_i$  is given by

$$S_i = \frac{\pi d_i^2}{4}, \quad (4)$$

where the inner diameter  $d_i$  is calculated by Eq.(3). From Fig. 3, it is found that the gradient  $\Delta p_i / \Delta d_o$  of the inner pressure varies as the cross sectional area  $S_i$  is changed.

Figure 5 shows the incremental elastic modulus  $H(p_i)$ , obtained from the gradient  $\Delta p_i / \Delta d_o$  of Fig. 3. It is found that the incremental elastic modulus  $H(p_i)$  of

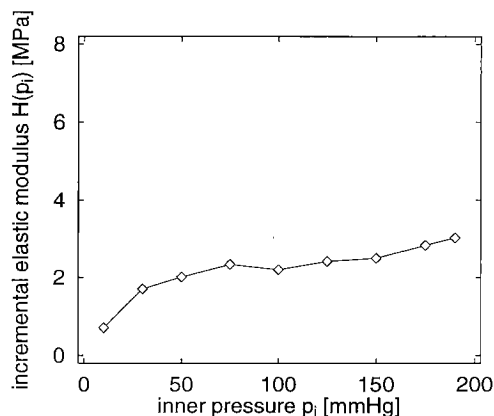


Fig. 5 Dependence of the incremental elastic modulus  $H(p_i)$  on the inner pressure  $p_i$ .

the silicone rubber tube gradually increases as the inner pressure  $p_i$  is increased. Thus, the incremental elastic modulus  $H(p_i)$  of the specimen markedly depends on the inner pressure  $p_i$ .

### 3.2 Pulse Wave Velocity $c_0$

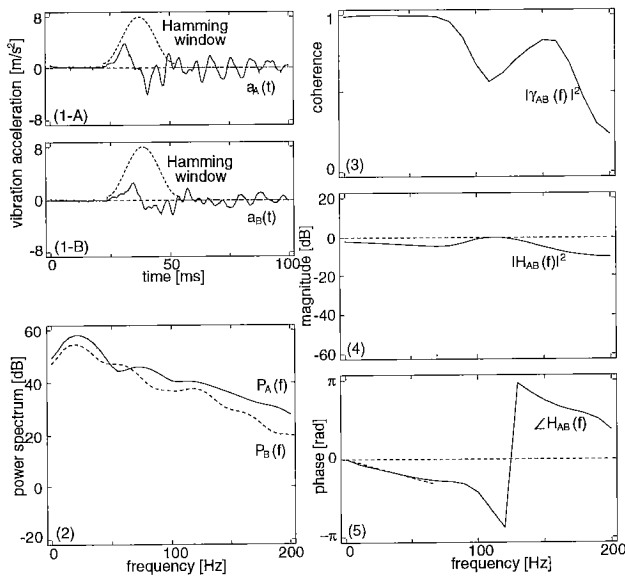
For the same silicone rubber tube as in the previous measurements, the pulse wave velocity  $c_0$  is measured to evaluate its dependence on the inner pressure  $p_i(t)$ . The distance  $d_{AB}$  between the two points A and B is 46.8 mm, and the sampling frequency is 5 kHz.

Figure 6 shows the results obtained by applying spectrum analysis to the resultant acceleration signals  $a_A(t)$  and  $a_B(t)$  when the diastolic pressure  $p_d$  is 50 mmHg and the pulse pressure  $p_p$  is 100 mmHg. Figure 6(1) shows the resultant acceleration signals  $a_A(t)$  and  $a_B(t)$ . Figure 6(2) shows that the power spectra  $P_A(f)$  and  $P_B(f)$  of  $a_A(t)$  and  $a_B(t)$ . Figure 6(3) shows the magnitude-squared coherence function  $|\gamma_{AB}(f)|^2$ . Figure 6(4) shows the squared magnitude  $|H_{AB}(f)|^2$  of the transfer function. Figure 6(5) shows the phase  $\angle H_{AB}(f)$  of the transfer function. It is confirmed that the transfer system of the local area between points A and B is linear because the magnitude-squared coherence function  $|\gamma_{AB}(f)|^2$  is almost 1 in the frequency range from d.c. to 70 Hz. From the gradient  $d\angle H_{AB}(f)/df$  of the phase of the transfer function in this frequency range (broken line in Fig. 6(5), which is obtained by using the least mean square method), the delay time  $\tau_{AB}$  between two points A and B is obtained by

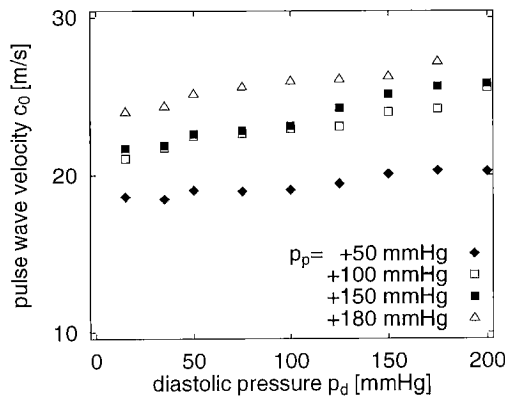
$$\tau_{AB} = -\frac{1}{2\pi} \frac{d}{df} \angle H_{AB}(f). \quad (5)$$

Thus, the obtained pulse wave velocity is  $c_0 = 22.4$  m/s.

The dependence of the pulse wave velocity  $c_0$  on the diastolic pressure  $p_d$  is shown in Fig. 7. It is found that the pulse wave velocity  $c_0$  gradually increases as the diastolic pressure  $p_d$  is increased.



**Fig. 6** The results of the spectrum analysis of the resultant acceleration signals with the diastolic pressure  $p_d = 50$  mmHg and the pulse pressure  $p_p = 100$  mmHg. (1) The resultant vibration signals  $a_A(t)$  and  $a_B(t)$ . (2) The power spectra  $P_A(f)$  and  $P_B(f)$  of  $a_A(t)$  and  $a_B(t)$ . (3) The magnitude-squared coherence function  $|\gamma_{AB}(f)|^2$ . (4) The magnitude of the transfer function  $|H_{AB}(f)|^2$  from measured point A to B. (5) Phase  $\angle H_{AB}(f)$  of the transfer function.

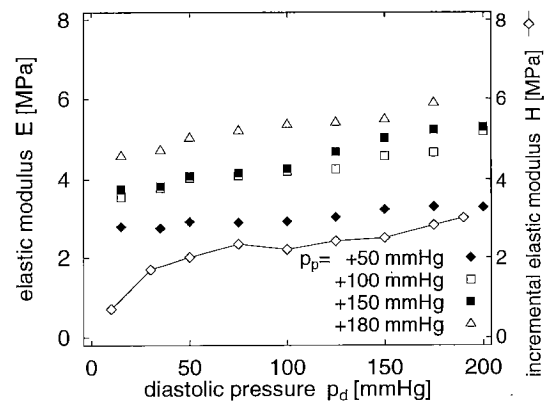


**Fig. 7** Dependence of the pulse wave velocity  $c_0$  on the diastolic pressure  $p_d$ .

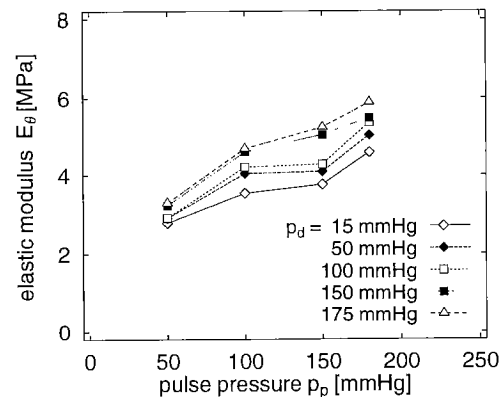
### 3.3 Dependence of Elastic Moduli $H(p_i)$ and $E$ on Inner Pressure $p_i(t)$

The obtained values of the elastic moduli  $H(p_i)$  and  $E$  are summarized in Fig. 8. In Fig. 8, Young's modulus  $E$  is obtained from Eq. (1), where the inner radius  $r$  of the specimen is 6.0 mm, the thickness  $h$  of the tube wall is 2.0 mm, and the mass density  $\rho$  of the inner fluid is  $1.0 \times 10^3$  kg/m<sup>3</sup>. It is clear that Young's modulus  $E$  gradually increases as the diastolic pressure  $p_d$  and the pulse pressure  $p_p$  are increased.

Figure 9 shows that the dependence of Young's modulus  $E$  on the pulse pressure  $p_p$  for various values of the diastolic pressure  $p_d$ . Moreover, the dependence of



**Fig. 8** Dependence of the elastic moduli  $H(p_i)$  and  $E$  on the diastolic pressure  $p_d$  and the pulse pressure  $p_p$ .



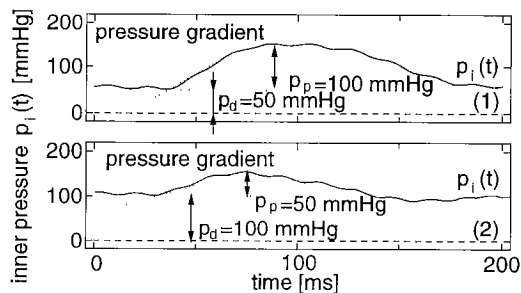
**Fig. 9** Dependence of Young's modulus  $E$  on the pulse pressure  $p_p$  and the diastolic pressure  $p_d$ .

Young's modulus  $E$  on the diastolic pressure  $p_d$  slightly increases with the pulse pressure  $p_p$ .

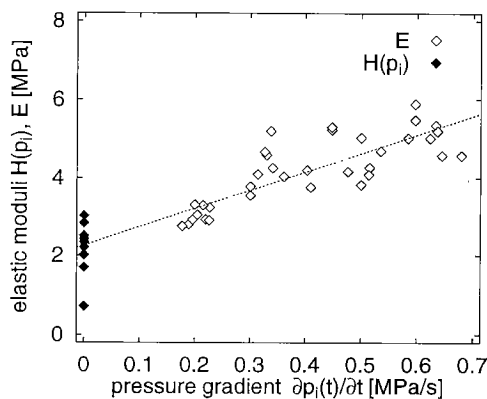
Furthermore, the obtained Young's modulus  $E$  is larger than the resultant incremental elastic modulus  $H(p_i)$  for the diastolic pressure  $p_d$  ranging from 15 to 200 mmHg. This relationship between  $E$  and  $H(p_i)$  is naturally explained by the following. The dynamic elastic modulus is always larger than the static one. The incremental elastic modulus  $H(p_i)$  is measured for statically applied stress; on the other hand, Young's modulus  $E$  is measured for dynamically applied stress. Thus, it is a natural consequence that Young's modulus  $E$  is larger than the incremental elastic modulus  $H(p_i)$ .

### 4. Discussions

With reference to Fig. 8, when the diastolic pressure  $p_d$  is 100 mmHg and the pulse pressure  $p_p$  is 50 mmHg, Young's modulus  $E$  is equal to 2.91 MPa; when  $p_d$  is 50 mmHg and  $p_p$  is 100 mmHg, however,  $E$  is equal to 4.04 MPa. Our major concern is what causes this difference. It can be explained as being the result of the waveform of the inner pressure  $p_i(t)$  and the pressure gradient  $\partial p_i(t)/\partial t$  at systole. Figure 10 shows the



**Fig. 10** Waveform of the inner pressure  $p_i(t)$  and the pressure gradient  $\partial p_i(t)/\partial t$  at systole. (1) The diastolic pressure  $p_d$  is 50 mmHg and the pulse pressure  $p_p$  is 100 mmHg. (2) The diastolic pressure  $p_d$  is 100 mmHg and the pulse pressure  $p_p$  is 50 mmHg.



**Fig. 11** Dependence of the elastic moduli  $H(p_i)$  and  $E$  on the pressure gradient  $\partial p_i(t)/\partial t$  at systole.

waveform of the inner pressure  $p_i(t)$  and its gradient  $\partial p_i(t)/\partial t$  by dashed line. For Figs.10(1) and 10(2), the systolic pressure, which is the sum of the diastolic pressure  $p_d$  and the pulse pressure  $p_p$  is the same, although, the pulse pressure  $p_p$  is different.

From various values of the diastolic pressure  $p_d$  and the pulse pressure  $p_p$ , the pressure gradient  $\partial p_i(t)/\partial t$  at systole is determined by the least square fitting to each measured waveform of the inner pressure  $p_i(t)$ . From Fig.8, the Young's modulus  $E$  is also obtained at each measurement with various values of the pressure. Thus the relationship between the  $\partial p_i(t)/\partial t$  and  $E$  is obtained. Figure 11 shows the dependence of Young's modulus  $E$  on the pressure gradient  $\partial p_i(t)/\partial t$ . In Fig.11, the measured plot points at  $\partial p_i(t)/\partial t = 0$  show the incremental elastic modulus  $H(p_i)$ . The broken line is obtained by the least squared fitting. Young's modulus  $E$  markedly increases as the pressure gradient  $\partial p_i(t)/\partial t$  is increased at systole because the relationship between the stress and the strain on the viscoelastic medium depends not only on the strain but also on the strain velocity.

## 5. Conclusions

In this paper, we measured the pulse wave velocity  $c_0$  and studied how Young's modulus  $E$  varies with various inner pressure  $p_i$ . The measurements were done with a silicone rubber tube, which has non-linearity on the stress-strain relationship. These results led to the conclusion that Young's modulus  $E$  estimated from the pulse wave velocity  $c_0$  depends on the inner pressure  $p_i$ . The inner pressure  $p_i$  varies even in the period of one heartbeat. From our study, it was shown that not only the diastolic pressure  $p_d$  but also the pulse pressure  $p_p$  and the pressure gradient  $\partial p_i(t)/\partial t$  at systole contribute to Young's modulus  $E$  obtained from the measurement of the pulse wave velocity  $c_0$ .

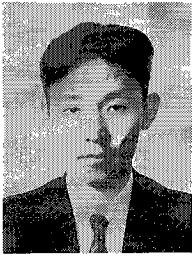
We used a small pressure detector and simultaneously measured the inner pressure  $p_i(t)$  at the point of measurement, though in *in vivo* measurement, such an invasive method is not desirable. Consequently, when Young's modulus  $E$  obtained from the measurement of the pulse wave velocity  $c_0$  is employed as a stiffness index of the arterial wall, it is important to correct the inner pressure  $p_i(t)$  not only by the diastolic pressure  $p_d$  but also by the pulse pressure  $p_p$  and the pressure gradient  $\partial p_i(t)/\partial t$  at systole.

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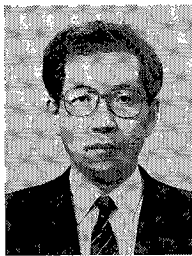
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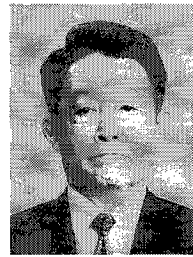
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